



Modeling of Turbulent Radiative Shocks with Applications to High Energy Density Physics and Astrophysics

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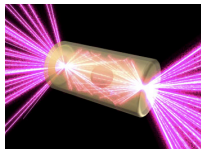
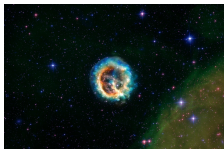
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Investigation models turbulent radiation hydrodynamics in the diffusion approximation and evaluates its effects on radiative blast waves

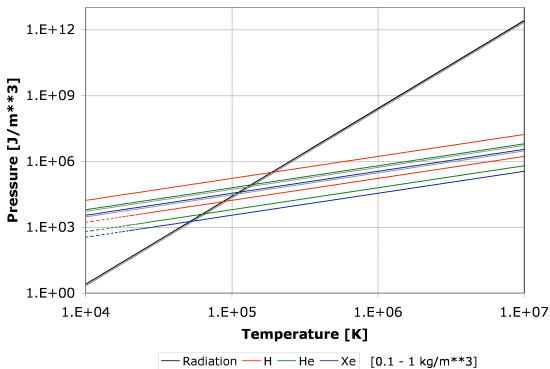
- Radiation transport, shock physics, and turbulence are intimately coupled in several HEDP and astrophysical environments
 - Supernovae, competing processes in stellar life cycles, black hole dynamics
 - Z-pinchs, high-energy laser experiments



- Blast waves created by such phenomena are susceptible to instabilities
 - Rayleigh-Taylor, Kelvin-Helmholtz, Richtmyer-Meshkov
- Theoretical and experimental studies typically focus on one or two of the processes: radiation, shock physics, turbulence
- This study models radiation hydrodynamics via equilibrium diffusion and turbulence by a Reynolds-averaged Navier-Stokes (RANS) model

Radiation fields directly influence hydrodynamics in extreme temperature and pressure environments

- Radiation to hydrodynamic pressure ratio = $a_R T^4 / (3\rho c_s^2)$



- Radiation quickly dominates system as temperature increases
 - $\frac{p_M}{p_R}(T = 10^6 K) \approx 5.95 \times 10^{-3}$, $\frac{p_M}{p_R}(T = 10^7 K) \approx 6.55 \times 10^{-6}$

Reynolds and Favre decompositions along with gradient-diffusion approximations are used to provide closed turbulent transport equations

- Reynolds and Favre averaging can be expressed as ordinary and density-weighted temporal means, respectively

$$\bar{\phi} = \lim_{\tau \rightarrow \infty} \frac{1}{\tau} \int_t^{t+\tau} \phi(\mathbf{x}, t) dt, \quad \tilde{\varphi} = \frac{1}{\bar{\rho}} \lim_{T \rightarrow \infty} \frac{1}{T} \int_t^{t+T} \rho(\mathbf{x}, t) \varphi(\mathbf{x}, t) dt$$

- Reynolds and Favre decompositions are given by:
 - $\rho = \bar{\rho} + \rho'$, $\rho = \bar{\rho} + \rho'$, $E_R = \bar{E}_R + E'_R$, $F_j = \bar{F}_j + F'_j$
 - $v_j = \tilde{v}_j + v'_j$, $U = \tilde{U} + U''$, $T = \tilde{T} + T''$
- Averaging system of interest and using decompositions leads to fluctuating correlations closed via gradient-diffusion closures
- Gradient-diffusion approximation uses turbulent kinetic energy, K , and dissipation rate, ϵ , to form the turbulent viscosity needed for the closures

$$\nu_t = C_\mu \frac{K^2}{\epsilon} = \frac{\mu_t}{\bar{\rho}}$$

Turbulent radiative gas dynamics is achieved by Reynolds averaging equilibrium diffusion model and generalizing gradient-diffusion closures

- Given total energy $\bar{\rho} \tilde{\mathcal{E}} = \bar{\rho} (\tilde{v}^2/2 + \tilde{U} + K) + \bar{E}_R$, total pressure $\bar{p}^* = \bar{p}_M + \bar{p}_R$, Reynolds stress tensor τ_{ij} , and radiative pressure dilatation Π^* , the first five model equations are

$$\text{Mass} \quad \frac{\partial \bar{\rho}}{\partial t} + \frac{\partial}{\partial x_j} (\bar{\rho} \tilde{v}_j) = 0$$

$$\text{Momentum} \quad \frac{\partial}{\partial t} (\bar{\rho} \tilde{v}_i) + \frac{\partial}{\partial x_j} (\bar{\rho} \tilde{v}_i \tilde{v}_j) = \bar{\rho} g_i - \frac{\partial \bar{p}^*}{\partial x_i} - \frac{\partial \tau_{ij}}{\partial x_j}$$

$$\text{Total Energy} \quad \frac{\partial}{\partial t} (\bar{\rho} \tilde{\mathcal{E}}^*) + \frac{\partial}{\partial x_j} [(\bar{\rho} \tilde{\mathcal{E}}^* + \bar{p}^*) \tilde{v}_j] = \bar{\rho} g_i \tilde{v}_i - \frac{\partial}{\partial x_j} \left[\frac{(\bar{p}^* + \bar{E}_R) \nu_t}{\sigma_\rho \bar{\rho}} \frac{\partial \bar{\rho}}{\partial x_j} \right]$$

$$- \frac{\partial}{\partial x_j} (\tau_{ij} \tilde{v}_i) + \frac{\partial}{\partial x_j} \left(\frac{\mu_t}{\sigma_U} \frac{\partial \tilde{U}}{\partial x_j} + \frac{\mu_t}{\sigma_K} \frac{\partial K}{\partial x_j} \right) + \frac{\partial}{\partial x_j} \left(\frac{4}{3} \frac{\nu_t}{\sigma_{E_R}} \frac{\partial \bar{E}_R}{\partial x_j} \right) - \frac{\partial \bar{F}_j^n}{\partial x_j}$$

$$\text{Turbulent K Energy} \quad \frac{\partial}{\partial t} (\bar{\rho} K) + \frac{\partial}{\partial x_j} (\bar{\rho} K \tilde{v}_j) = - \frac{\nu_t}{\sigma_\rho \bar{\rho}} \frac{\partial \bar{\rho}}{\partial x_j} \frac{\partial \bar{p}^*}{\partial x_j} - \tau_{ij} \frac{\partial \tilde{v}_i}{\partial x_j} - \bar{\rho} \epsilon + \Pi^* + \frac{\partial}{\partial x_j} \left(\frac{\mu_t}{\sigma_K} \frac{\partial K}{\partial x_j} \right)$$

$$\text{Dissipation Rate} \quad \frac{\partial}{\partial t} (\bar{\rho} \epsilon) + \frac{\partial}{\partial x_j} (\bar{\rho} \epsilon \tilde{v}_j) = - \frac{\epsilon}{K} \left[C_{\epsilon 0} \frac{\nu_t}{\sigma_\rho \bar{\rho}} \frac{\partial \bar{\rho}}{\partial x_j} \frac{\partial \bar{p}^*}{\partial x_j} + C_{\epsilon 1} \tau_{ij} \frac{\partial \tilde{v}_i}{\partial x_j} + C_{\epsilon 2} \bar{\rho} \epsilon - C_{\epsilon 3} \Pi^* \right]$$

$$+ \frac{\partial}{\partial x_j} \left(\frac{\mu_t}{\sigma_\epsilon} \frac{\partial \epsilon}{\partial x_j} \right)$$

Turbulence contributions introduced via mean radiative flux introduce need for transport equations for density and temperature variances

- Classical and mean radiative fluxes with opacity model $\Sigma_A(\rho, T)$ for $1 \leq n \leq 3$ are

$$F_j^n = \frac{c}{3 \Sigma_A(\rho, T)} \frac{\partial E_R}{\partial x_j}, \quad \Sigma_A(\rho, T) = \beta \frac{\rho}{T^n}$$

$$\bar{F}_j^{n=1} = -\frac{a_R c \tilde{T}}{3 \beta \bar{\rho}} \left[\left(1 + 2 C_T \frac{\sqrt{\rho'^2 \widetilde{T''^2}}}{\bar{\rho} \tilde{T}} + \frac{\rho'}{\bar{\rho}^2} \right) \frac{\partial \tilde{T}^4}{\partial x_j} - \frac{2}{\lambda_\rho \bar{\rho}} \sqrt{\frac{2 \rho'^2}{\pi}} \tilde{T}^4 \right]$$

$$-\frac{a_R c}{3 \beta \bar{\rho}} \left[\frac{\partial}{\partial x_j} \left(\tilde{T}^5 - \tilde{T} \tilde{T}^4 - C_T \frac{\sqrt{\rho'^2 \widetilde{T''^2}}}{\bar{\rho}} \tilde{T}^4 \right) - \frac{2}{\lambda_T} (\tilde{T}^5 - \tilde{T}^4 \tilde{T}) + C_T \tilde{T}^4 \frac{\partial}{\partial x_j} \left(\frac{\sqrt{\rho'^2 \widetilde{T''^2}}}{\bar{\rho}} \right) \right]$$

- Compressible turbulent and PDF closures are used in density variance, $\overline{\rho'^2}$, and temperature variance, $\widetilde{T''^2}$, transport equations development

$$\text{Dens. Var.} \quad \frac{\partial \overline{\rho'^2}}{\partial t} + \frac{\partial}{\partial x_j} (\overline{\rho'^2} \tilde{v}_j) = \frac{2 \nu_t}{\sigma_\rho} \left(\frac{\partial \bar{\rho}}{\partial x_j} \right)^2 - \overline{\rho'^2} \frac{\partial \tilde{v}_j}{\partial x_j} - C_{\rho^2} \frac{\epsilon}{K} \overline{\rho'^2} - \frac{2 \bar{\rho}^2 \Pi^*}{\gamma \bar{\rho}} + \frac{\partial}{\partial x_j} \left(\frac{\nu_t}{\sigma_{\rho^2}} \frac{\partial \overline{\rho'^2}}{\partial x_j} \right)$$

$$\text{Temp. Var.} \quad \frac{\partial}{\partial t} (\bar{\rho} \widetilde{T''^2}) + \frac{\partial}{\partial x_j} (\bar{\rho} \widetilde{T''^2} \tilde{v}_j) = 2 \left[\frac{\mu_t}{\sigma_U} \left(\frac{\partial \tilde{T}}{\partial x_j} \right)^2 - (\gamma - 1) \bar{\rho} \widetilde{T''^2} \frac{\partial \tilde{v}_j}{\partial x_j} \right]$$

$$-2(\gamma - 1) C_T \frac{\epsilon}{K} \tilde{T} \sqrt{\overline{\rho'^2 \widetilde{T''^2}}} + \frac{\partial}{\partial x_j} \left(\frac{\mu_t}{\sigma_U} \frac{\partial \widetilde{T''^2}}{\partial x_j} \right)$$



Rankine-Hugoniot jump relations ensure total mass, momentum, and energy conservation and provide post shock relations

- Exact relations for profiles behind strong turbulent-radiative shocks as functions of shock speed, \tilde{v}_s , are given by

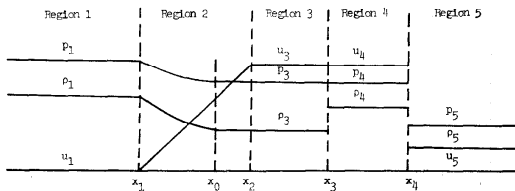
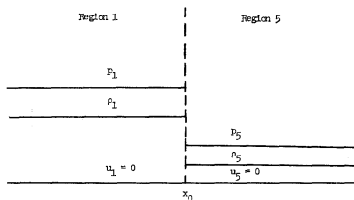
$$\begin{aligned}
 \text{Density : } \quad \frac{\bar{\rho}_2}{\bar{\rho}_1} &= \frac{(\gamma + 1)\bar{\rho}_2^* + (\gamma - 1)\tau_2 + 2(4 - 3\gamma)\bar{\rho}_{R,2}}{(\gamma - 1)\bar{\rho}_2^*} \left[1 + \frac{2}{\bar{\rho}_2^*} \left(\frac{\tau_2}{2} - \bar{\rho}_1 K_2 - \frac{\Gamma_2^*}{\tilde{v}_1} \right) \right]^{-1} \\
 \text{Velocity : } \quad \tilde{v}_2 &= \tilde{v}_s \left\{ 1 - \frac{(\gamma - 1)\bar{\rho}_2^*}{(\gamma + 1)\bar{\rho}_2^* + (\gamma - 1)\tau_2 + 2(4 - 3\gamma)\bar{\rho}_{R,2}} \left[1 + \frac{2}{\bar{\rho}_2^*} \left(\frac{\tau_2}{2} - \bar{\rho}_1 K_2 - \frac{\Gamma_2^*}{\tilde{v}_s} \right) \right] \right\} \\
 \text{Pressure : } \quad \bar{p}_2^* &= \bar{\rho}_1 \tilde{v}_s^2 \left\{ 1 - \frac{(\gamma - 1)\bar{\rho}_2^*}{(\gamma + 1)\bar{\rho}_2^* + (\gamma - 1)\tau_2 + 2(4 - 3\gamma)\bar{\rho}_{R,2}} \left[1 + \frac{2}{\bar{\rho}_2^*} \left(\frac{\tau_2}{2} - \bar{\rho}_1 K_2 - \frac{\Gamma_2^*}{\tilde{v}_s} \right) \right] \right\} \\
 &\quad - \tau_2 \\
 \Gamma^* &= \frac{(\bar{p}^* + 3\bar{p}_R)\nu_t}{\sigma_\rho \bar{\rho}} \frac{\partial \bar{p}}{\partial x_j} - \frac{\mu_t}{\sigma_U} \frac{\partial \tilde{U}}{\partial x_j} - \frac{\mu_t}{\sigma_K} \frac{\partial K}{\partial x_j} - \frac{4\nu_t}{\sigma_{E_R}} \frac{\partial \bar{p}^*}{\partial x_j} + \bar{F}_{i,F}^n
 \end{aligned}$$

- As a check, results for a strong classical shock are obtained when removing turbulence and radiative effects

$$\frac{\rho_2}{\rho_1} = \frac{\gamma + 1}{\gamma - 1} \quad , \quad v_2 = \frac{2 v_s}{\gamma + 1} \quad , \quad p_2 = \frac{2 \rho_1 v_s^2}{\gamma + 1}$$

Weighted Essentially Non Oscillatory (WENO) and Riemann solvers will be used to simulate proposed turbulent radiation hydrodynamics model

- Sod reference problem is used to test early stage computational work
- Problem depicts two regions ($\gamma = 1.4$) under conditions:
 - $\rho_1 = 1.0$, $p_1 = 1.0$, $v_1 = 0$ || $\rho_5 = 0.125$, $p_5 = 0.10$, $v_5 = 0$



Ongoing and future work, and special thanks

- Physics of underlying turbulent radiative shocks has been investigated
 - An equilibrium diffusion model describes radiation hydrodynamics
 - A four-equation Reynolds-averaged Navier-Stokes (RANS) model is used to describe turbulence effects
 - Gradient-diffusion and similarity closures were generalized to account for radiative effects
- WENO methods and approximate Riemann solvers will be used for conducting numerical investigations
- Particular interest lies in studying these processes in planar, cylindrical, and spherical geometries for applications relevant to supernovae, black hole dynamics, high-energy laser experiments, and Z-pinchs
- Propose experiments that can be used to verify this model

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